

Appendix A

Room-temperature Mössbauer spectrum of zirconolite

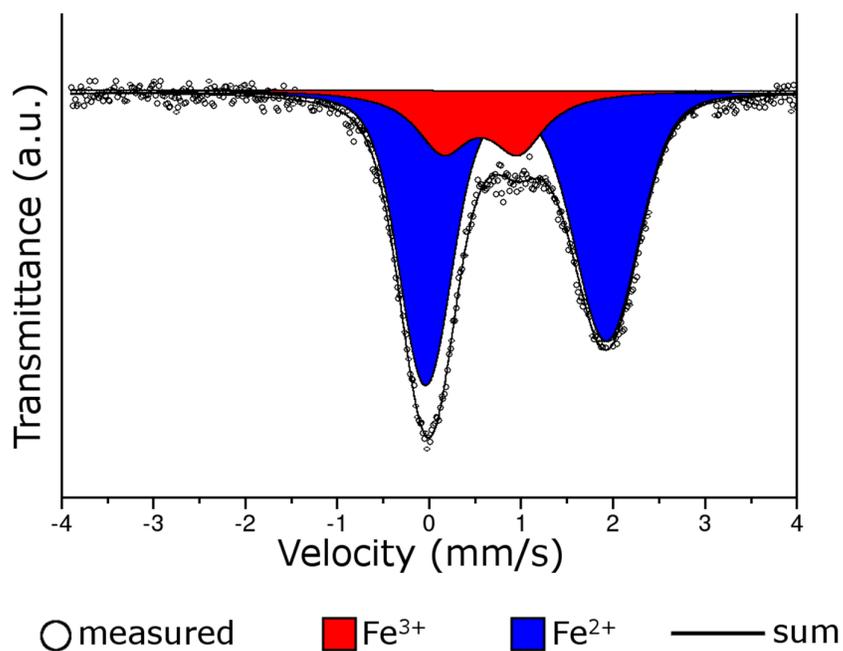


Figure A1. Room-temperature Mössbauer spectrum of zirconolite

Table A1. Quantitative parameters of the Mössbauer spectrum of zirconolite from Fig. A1

Isomer shift	Quadrupole splitting	Full width	Area	Assignment
mm/s	mm/s	mm/s	%	
0.564	0.819	0.701	20.6	Fe ³⁺
0.949	1.967	0.226	79.4	Fe ²⁺

Appendix B

X-ray powder diffraction patterns of unannealed and thermally annealed zirconolite

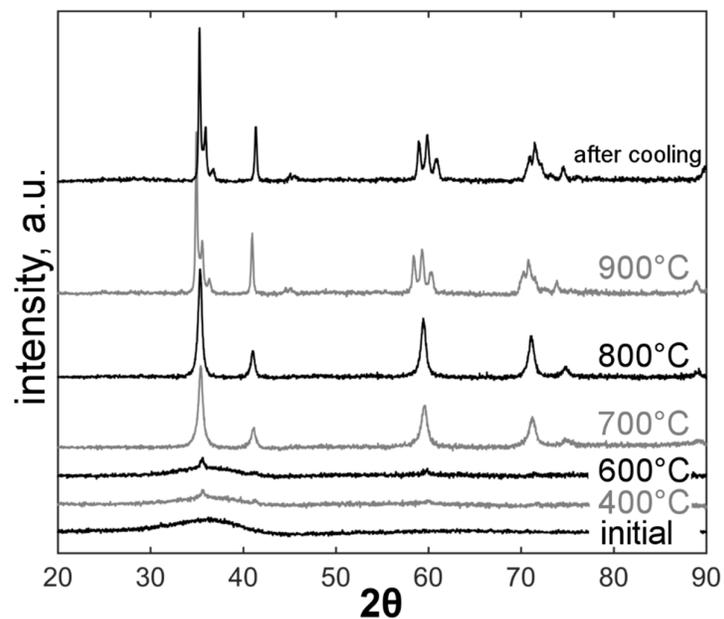


Figure B2. X-ray powder diffraction patterns of unannealed and thermally annealed zirconolite from the LPC. Variation of the diffraction patterns with increasing temperature due to recrystallisation of initially radiation-damaged mineral.

Appendix C

Estimation of iron oxidation state ($X_{Fe^{3+}}$) or $X_{Me^{3+}}$ from other composition variables: X_{REE^*} and $X_{Me^{5+}}$

The Equation 1, $X_{Me^{3+}} = 2 - 2X_{REE} - 3X_{Me^{5+}}$, introduced in the article, is **valid for a sort of zirconolite**, which can be expressed by formula $(Ca,REE)_2Zr_2(Ti,Me^{5+})_3(Me^{2+},Me^{3+})O_{14}$, i.e. free of actinides and containing 1 atom $Me^{2+} + Me^{3+}$ per 14 O. The composition variables in Eq. 1 are as follows:

$$X_{Me^{3+}} = Me^{3+}/(Me^{2+} + Me^{3+}); X_{REE} = REE/(Ca + REE); X_{Me^{5+}} = Me^{5+}/(Ti + Me^{5+})$$

Note: To derive Eq. 1, compositions of three endmembers suggested in this study, $Ca_2Zr_2Me^{5+}_2TiMe^{2+}O_{14}$, $Ca_2Zr_2Ti_2Me^{5+}Me^{3+}O_{14}$, $CaREEZr_2Ti_3Me^{3+}O_{14}$, were projected as points in a 3-dimensional (X_{REE} , $X_{Me^{5+}}$, $X_{Me^{3+}}$) linear Cartesian space. These points were fitted by a general form of the equation of a plane $a * X_{REE} + b * X_{Me^{5+}} + c * X_{Me^{3+}} + d = 0$ to determine coefficients a , b , c , d which are $\frac{2}{3}$, 1 , $\frac{1}{3}$, $-\frac{2}{3}$.

For actinide-bearing zirconolite and zirconolite containing ≤ 1 $Me^{2+} + Me^{3+}$ atom per 14 O, i.e. compositions expressed as $(Ca,REE,ACT)_2Zr_2(Ti,Me^{5+})_3(Me^{2+},Me^{3+},Ti)O_{14}$, the calculation is modified to consider participation of ideal zirconolite, $Ca_2Zr_2Ti_4O_{14}$, and $CaACTZr_2Ti_3Me^{2+}O_{14}$. The fraction of the former is subtracted from other endmembers (the variable X_{id} is a fraction of uncoupled ideal zirconolite in the solid solution), while the latter is projected at the same point as $REE_2Zr_2Ti_3Me^{2+}O_{14}$ in Fig. 11. For this extended system, the calculation is as follows:

$$X_{Me^{3+}} = 2 - 2X_{REE^*} - 3X_{Me^{5+}} \quad (2)$$

The modified variables are expressed as follows:

$$X_{REE^*} = \frac{(REE+2ACT)}{[REE+ACT+Ca-2X_{id}]} \quad (3)$$

$$X_{Me^{5+}} = \frac{Me^{5+}}{[Me^{5+}+Ti-4X_{id}]} \quad (4)$$

$$X_{id} = \frac{4(Ti+Me^{5+})}{(Me^{2+}+Me^{3+}+Me^{5+}+Ti)} - 3 \quad (5)$$