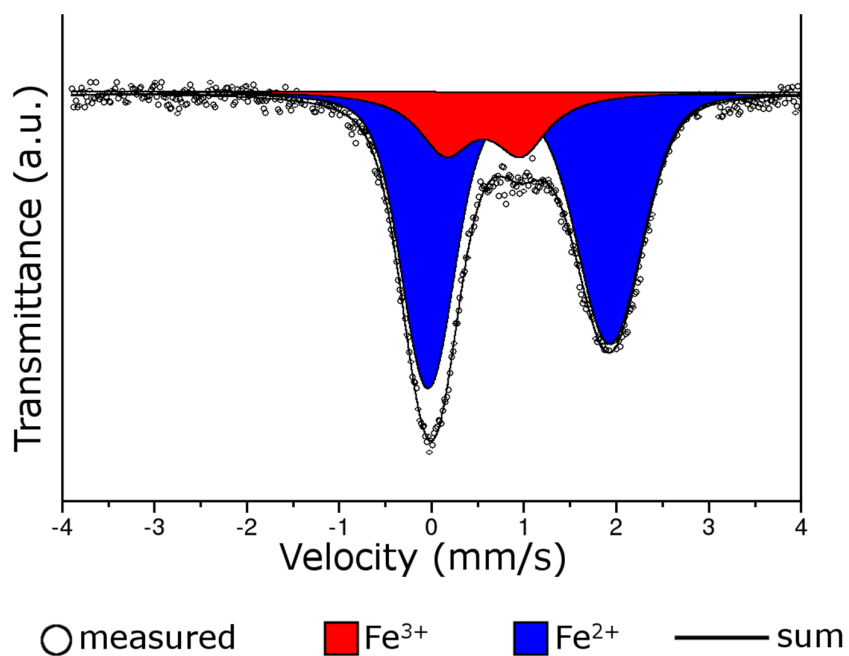


## Appendix A

### Room-temperature Mössbauer spectrum of zirconolite



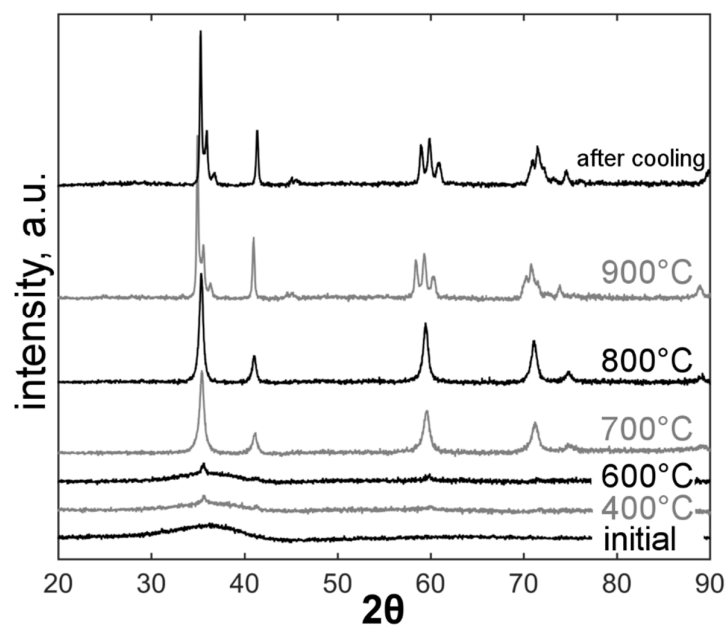
**Figure A1.** Room-temperature Mössbauer spectrum of zirconolite

**Table A1.** Quantitative parameters of the Mössbauer spectrum of zirconolite from Fig. A1

Isomer shift	Quadrupole splitting	Full width	Area	Assignment
mm/s	mm/s	mm/s	%	
0.564	0.819	0.701	20.6	Fe <sup>3+</sup>
0.949	1.967	0.226	79.4	Fe <sup>2+</sup>

## Appendix B

### X-ray powder diffraction patterns of unannealed and thermally annealed zirconolite



**Figure B2.** X-ray powder diffraction patterns of unannealed and thermally annealed zirconolite from the LPC. Variation of the diffraction patterns with increasing temperature due to recrystallisation of initially radiation-damaged mineral.

## Appendix C

### Estimation of iron oxidation state ( $X_{Fe^{3+}}$ ) or $X_{Me^{3+}}$ from other composition variables: $X_{REE^*}$ and $X_{Me^{5+}}$

The Equation 1,  $X_{Me^{3+}} = 2 - 2X_{REE} - 3X_{Me^{5+}}$ , introduced in the article, is **valid for a sort of zirconolite**, which can be expressed by formula  $(Ca,REE)_2Zr_2(Ti,Me^{5+})_3(Me^{2+},Me^{3+})O_{14}$ , i.e. free of actinides and containing 1 atom  $Me^{2+} + Me^{3+}$  per 14 O. The composition variables in Eq. 1 are as follows:

$$X_{Me^{3+}} = Me^{3+}/(Me^{2+} + Me^{3+}); X_{REE} = REE/(Ca + REE); X_{Me^{5+}} = Me^{5+}/(Ti + Me^{5+})$$

Note: To derive Eq. 1, compositions of three endmembers suggested in this study,  $Ca_2Zr_2Me^{5+}_2TiMe^{2+}O_{14}$ ,  $Ca_2Zr_2Ti_2Me^{5+}Me^{3+}O_{14}$ ,  $CaREEZr_2Ti_3Me^{3+}O_{14}$ , were projected as points in a 3-dimensional ( $X_{REE}$ ,  $X_{Me^{5+}}$ ,  $X_{Me^{3+}}$ ) linear Cartesian space. These points were fitted by a general form of the equation of a plane  $a * X_{REE} + b * X_{Me^{5+}} + c * X_{Me^{3+}} + d = 0$  to determine coefficients  $a$ ,  $b$ ,  $c$ ,  $d$  which are  $\frac{2}{3}$ ,  $1$ ,  $\frac{1}{3}$ ,  $-\frac{2}{3}$ .

For actinide-bearing zirconolite and zirconolite containing  $\leq 1$   $Me^{2+} + Me^{3+}$  atom per 14 O, i.e. compositions expressed as  $(Ca,REE,ACT)_2Zr_2(Ti,Me^{5+})_3(Me^{2+},Me^{3+},Ti)O_{14}$ , the calculation is modified to consider participation of ideal zirconolite,  $Ca_2Zr_2Ti_4O_{14}$ , and  $CaACTZr_2Ti_3Me^{2+}O_{14}$ . The fraction of the former is subtracted from other endmembers (the variable  $X_{id}$  is a fraction of uncoupled ideal zirconolite in the solid solution), while the latter is projected at the same point as  $REE_2Zr_2Ti_3Me^{2+}O_{14}$  in Fig. 11. For this extended system, the calculation is as follows:

$$X_{Me^{3+}} = 2 - 2X_{REE^*} - 3X_{Me^{5+}} \quad (2)$$

The modified variables are expressed as follows:

$$X_{REE^*} = \frac{(REE+2ACT)}{[REE+ACT+Ca-2X_{id}]} \quad (3)$$

$$X_{Me^{5+}} = \frac{Me^{5+}}{[Me^{5+}+Ti-4X_{id}]} \quad (4)$$

$$X_{id} = \frac{4(Ti+Me^{5+})}{(Me^{2+}+Me^{3+}+Me^{5+}+Ti)} - 3 \quad (5)$$